Amendments to the Specification:

Please replace the paragraph beginning at page 9, line 22 with the following amended paragraph:

Next, the image forming apparatus according to the present invention includes the above-mentioned image heating device according to the present invention. According to this configuration, an amount of heat generated in ~~an axis~~ the width direction can be regulated so as to have an arbitrary distribution corresponding to a width of a body to be heated and a temperature of the heat generating member. Moreover, the heat generation suppressing unit suppresses an amount of heat generated in the heat generating member in a center portion in the width direction, thereby allowing a simplified configuration and a reduced cost to be achieved. Further, in the case where the heat generation suppressing unit is operated, diffusion of magnetic flux into a wide area can be prevented.

Please replace the paragraph beginning at page 18, line 14 with the following amended paragraph:

In this embodiment, when passing a small-width paper sheet, the relay 8 is opened. In contrast to this, in the conventional image heating device shown in FIG. 23, when passing a small-width paper sheet, the ~~cancel coil~~ switching element 909 is switched on. As in the conventional technique, when the ~~cancel coil~~ switching element 909 is switched on in passing a small-width paper sheet, with a constant driving current applied to the excitation coil 904, a total amount of magnetic flux generated by the excitation coil 904 is decreased. Therefore, the inductance of the excitation coil 904 decreases, thereby

decreasing the load impedance of the excitation coil 904 with respect to the excitation circuit. This raises a possibility that an amount of a driving current that passes through the excitation coil 904 is increased, so that an amount of heat generated is increased. As described above, in the configuration shown in FIG. 23, when a small-width paper sheet is passed, while it is necessary to reduce an amount of heat generated, an amount of a driving current that passes through the excitation coil 904 is likely to be increased. This raises a necessity for an electric current controlling circuit that controls an increase in the driving current. Moreover, in this case, since a change in a target value of an amount of heat generated has a phase opposite to that of a change in an amount of heat generated caused by a variation in load impedance, a wide control range of the electric current is required. Thus, in order to realize such controlling, a complex and expensive device is required. In addition, in the case where this electric current controlling circuit does not operate properly, there is a possibility that a breakdown is caused in the excitation circuit and the excitation coil 904 due to an excessively large electric current.

Please replace the paragraph beginning at page 24, line 10 with the following amended paragraph:

The four movable arch cores 5d are of the same dimensions, formed of the same material and arranged at the same distance from each other as in the case of the arch cores 5b3 to 5b6 of Embodiment 1. These arch cores 5d have their upper faces fixed to the ~~holder 22~~ holder 21 so as to be held by the ~~holder 22~~ holder 21. Each of the feed screws 22 is threaded in an internal thread formed at each end of the ~~holder 22~~ holder 21, and an upper

end of the feed screw 22 is connected to a rotary mechanism that is not shown in the figure. The feed screws 22 are rotated so that the ~~holder 22~~ holder 21 and the movable arch cores 5d as a unit move up and down in a radial direction of the heat generating tube 1. In this case, a central core 5a, end cores 5c and arch cores 5b1, 5b2, 5b7 and 5b8 are stationary.

Please replace the paragraph beginning at page 25, line 19 with the following amended paragraph:

Therefore, when passing a maximum-width recording paper sheet, the four movable arch cores 5d in the center portion are moved to the distant position. When heating is performed in this state, magnetic flux that passes through ~~the movable coils 5d~~ the movable arch cores 5d is decreased, so that an amount of heat generated in the center portion is suppressed. Thus, a distribution of an amount of heat generated can be made uniform over the entire width of the heat generation tube 1, thereby allowing the whole heat generating tube 1 to be kept at substantially a uniform temperature.

Please replace the paragraph beginning at page 26, line 36 with the following amended paragraph:

Reference numeral 30 denotes a thin endless fixing belt. The fixing belt 30 is formed from a polyimide resin in which conductive powder is dispersed so that conductivity is imparted. The fixing belt 30 is formed of a 100-μm thick base material of a diameter of 45 mm with its surface coated with a 150-μm thick silicone rubber layer and a 20-μm

thick fluorocarbon resin layer as a mold releasing layer that is provided on the silicone rubber layer. However, the configuration of the ~~fixing belt 20~~ fixing belt 30 is not limited thereto. For example, as a material of the base material, a heat-resistant material of a fluorocarbon resin, PPS or the like in which powder of a conductive material is dispersed, and an extremely thin metal of nickel, stainless steel or the like that is formed by electroforming also can be used. Further, the mold releasing layer on the surface may be formed by coating of a single material or a combination of materials selected from resin or rubber materials having excellent mold releasability such as PTFE, PFA, FEP, fluorocarbon rubber or the like.

Please replace the paragraph beginning at page 29, line 10 with the following amended paragraph:

~~FIG. 12~~ FIG. 13 shows a basic circuit of a single-ended voltage-fed resonant inverter that is used in the excitation circuit 9. An alternating current from a commercial power source 40 is rectified in a rectifier circuit 41 and applied to the inverter. In the inverter, a high-frequency current is applied to the excitation coil 4 using a switching element 44 such as an IGBT (Insulated Gate Bipolar Transistor) and a resonant capacitor 43. Reference numeral 42 denotes a diode. In this embodiment, an alternating current having a maximum voltage amplitude of 650 V and a maximum current amplitude of 65 A is applied from the excitation circuit 9.

Please replace the paragraph beginning at page 30, line 33 with the following

amended paragraph:

Furthermore, the synchronization of switching of the switching element 8 with a variation in a high-frequency current supplied to the excitation coil 4 also can be achieved in the following manner. That is, the switching element 8 is switched over at a timing that is the same as the switching timing of a ~~switching element 44~~ switching element 8 for the inverter of the excitation circuit 9. In this case, it is not required that the switching element 44 be switched over at a timing that is exactly the same as the switching timing of the switching element 44, and the respective timings may be shifted by a predetermined time.